

BPhO Round 1 marking 2017

- Positive marking is the aim. Marks should be awarded for good physics, even if the reasoning does not follow the mark scheme. Alternative routes to the answers can be allowed.
 - Significant figures. A leeway of ± 1 sig fig is allowed; if the published solution gives 3, allow 2 or 4 in the students answer. This only applies to the final answers as intermediate answers may be recorded to greater precision to avoid rounding errors. Candidates should not lose more than 1 mark per question for this even if they have got it wrong in more than one place in the question (they might lose all their hard earned marks otherwise). Question 1 (a) is different in this respect as it is specifically about sf and dp.
 - Units should be given for the final answer. It may be that the unit is given a little earlier and that it does not appear on the very last line. Some allowance may be made if it is clear that the unit has been used a line or two earlier.
 - In one or two places the units are a required part of the answer for the mark, and so must be there.
 - Error carried forward (ecf) is allowed provided ridiculous results do not start appearing. A mark is lost for the initial mistake, but then they can carry on (if it is possible) to gain some of the subsequent marks.
 - You are not required to spend time deciphering scribble.
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- In some cases, the mark scheme allows for different methods of solution. You will need to award marks for these solutions, with a mark for each key step in heading for a solution. You cannot give more marks than is available.
 - The significant figures – although some details are given above, this is not a paper testing use of significant figures. Two sig figures in the answer to almost every question would be fine. I think you will find some inconsistencies in the solutions, with more figures given than might be justified.
 - There are a few questions in which two or at most three marks are awarded for working, whose details are not shown. For example, Qu 3 on the crane; there are a number of ways of getting the results, but students will generally not set out their path. Therefore, a mark for a sensible resolving, or taking moments about a point, etc. will contribute to the working marks; often students will get lost. You do not need to find the exact point at which they made a mistake. Wrong answer – they lose that mark. Some working heading in the right direction, one or two marks. Judgement is required, but not timewasting.
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- If stuck, email robin Hughes on rh584@cam.ac.uk and I will reply fairly quickly.

BPhO Round 1 2017.

①

Section 1.

Ques 1(a) $1 \frac{\text{foot}}{\text{ns}} = \frac{1}{3} \frac{\text{yd}}{\text{ns}}$

$$= \frac{1}{3} \times \frac{1}{1.094} \frac{\text{m}}{\text{ns}}$$

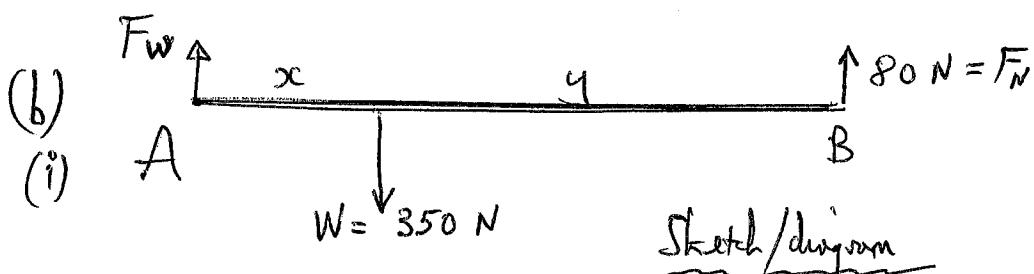
$$= 3.047 \times 10^{-8} \text{ m s}^{-1}$$

$$\text{Error} = \frac{3.047 - 3.000}{3.000}$$

✓
✓

* $\frac{1 - 0.9846}{3} = 1.54\%$
 only gain $\frac{2}{3}$ marks $= 1.564\%$
 $\underline{= 1.6\%}$

(3)



Moment about A ↑

$$5 \times 80 - 350 \cdot x = 0$$

$$x = \frac{400}{350} = \frac{8}{7} \text{ m}$$

$$= \underline{1.14 \text{ m}}$$

(ii)

$$x + y = 5.0 \text{ m}$$

$$y = \frac{27}{7} \text{ m} = 3.86 \text{ m}$$

Moments about B ↑

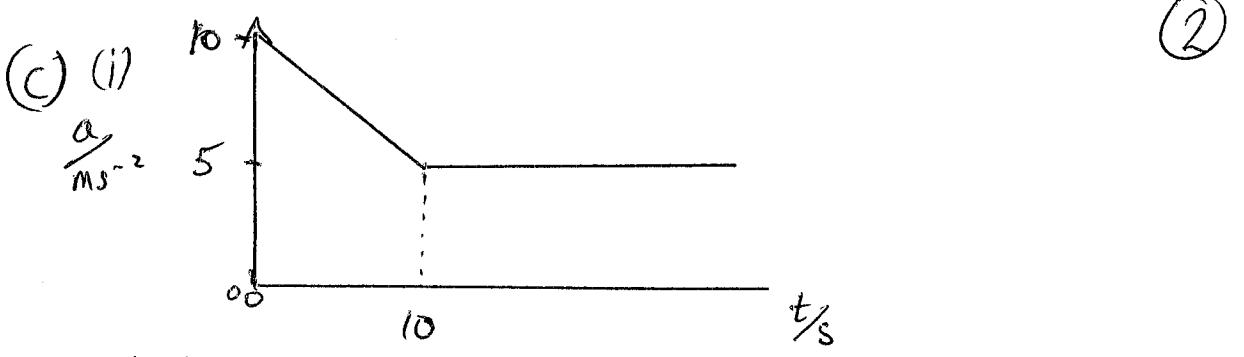
$$F_w \times 5 - 350 \times \frac{27}{7}$$

$$F_w = \underline{270 \text{ N}}$$

[or $F_w + 80 = 350$
 $\Rightarrow F_w = 270 \text{ N}$ ✓].

(5)

Answers as fractions, or to 2 ff. are ok.



Graphically.

change in velocity = area under a-t graph

In first 10s, average acceleration is 7.5 ms^{-2}

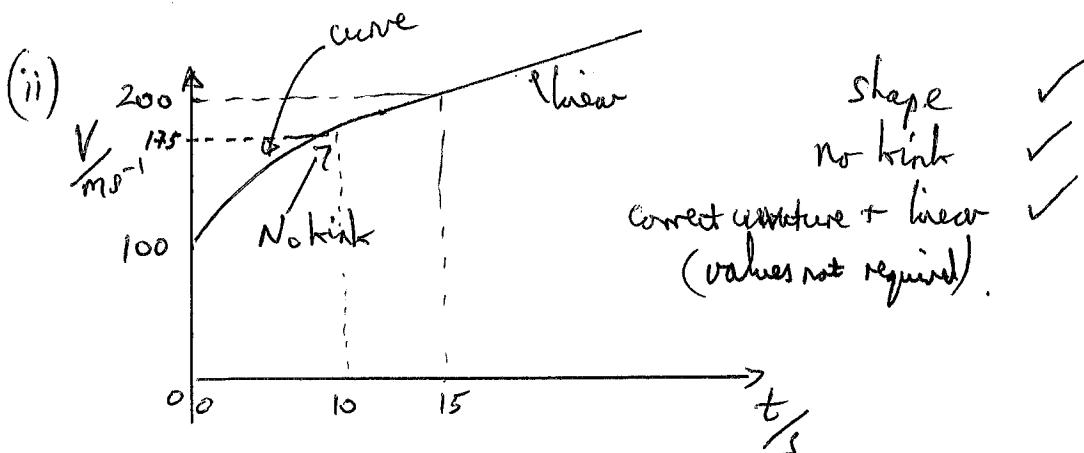
So change in velocity is 75 ms^{-1}

So, after 10s, the velocity is $100 + 75 = 175 \text{ ms}^{-1}$

To reach 200 ms^{-1} , an extra 25 ms^{-1} is needed

Constant acceleration of 5 ms^{-2} would take 5 s

which is 15 s after the start



or algebraically (7)

$$a = -\frac{1}{2}t + 10 \quad (\text{in SI units})$$

$$\int a dt = \int_0^{10} (-\frac{1}{2}t + 10) dt$$

$$V - 100 = \left[-\frac{1}{4}t^2 + 10t \right]_0^{10}$$

$$= 75 \text{ ms}^{-1}$$

$$V = 175 \text{ ms}^{-1}$$

} 4 marks

(3)

or by comparison with " $s = ut + \frac{1}{2}at^2$ " (const a)

$$V - u = at + \frac{1}{2} \left(\frac{da}{dt} \right) \cdot t^2 \quad (\text{const. } \frac{da}{dt} \text{ for } 10 \text{ s})$$

$$V - 100 = 10, 10 + \frac{1}{2} \left(-\frac{1}{2} \right) 10^2$$

$$= 100 - 25$$

$$\underline{V = 175 \text{ ms}^{-1}}$$

(4 marks)

or integrate from start., (4 marks)

$$V_f = 200 = 100 + \int_0^{10} (-kt + 10) dt + \int_{10}^t 5 dt$$

$$\frac{da}{dt} = k = \frac{(200-100)}{5} \therefore V_f = 100 \left(-\frac{1}{2} \frac{t^2}{2} + 10t \right) \Big|_0^{10} + 5(t-10)$$

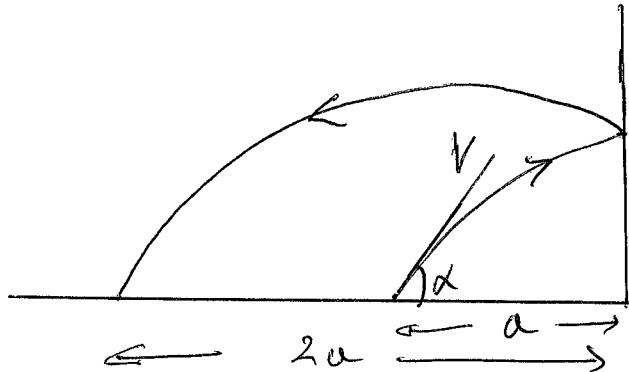
$$= -\frac{1}{2} \text{ ms}^{-2}$$

$$200 = 100 - 25 + 100 + 5t - 50$$

$$\underline{\underline{t = 15.3}}$$

(4)

(d)



Horizontal components : $V_{\text{before}} = V \cos \alpha$

$$V_{\text{after}} = e V_{\text{before}} = e V \cos \alpha$$

So, distance $a = t_1 \cdot V_{\text{before}}$ (time of flight to right, t_1)

and $2a = t_2 \cdot e V_{\text{before}}$ (..... to left, t_2)

Hence $t_2 = \frac{2}{e} \cdot t_1$ ($t_2 = 3t_1$)

The vertical velocity is unaffected by the collision.

So, total time in flight is $2 \times \frac{V_{\text{vertical}}}{g}$

$$\text{i.e. } t_1 + t_2 = \frac{2 V_{\text{vertical}}}{g}$$

$$\therefore \frac{2 V_{\text{vertical}}}{g} = \frac{a}{V_{\text{before}}} + \frac{2}{e} \cdot \frac{a}{V_{\text{before}}}$$

$$\frac{2 V^2 \sin \alpha \cdot \cos \alpha}{g} = \left(\frac{2}{e} + 1\right) a$$

$$V^2 \sin 2\alpha = \left(\frac{2}{e} + 1\right) g \cdot a$$

$$V^2 \sin 2\alpha = 4g a$$

Other idea: $\sqrt{V \sin \alpha} = \frac{1}{2} g t$ $t = \text{time of flight (no effect of wall)}$

$$14. \quad V \cos \alpha \cdot t_1 = a$$

$$\text{and } \frac{2}{3} V \cos \alpha \cdot t_2 = 2a$$

Knowing $t = t_1 + t_2 = \frac{2a \cdot 3}{2V \cos \alpha} + \frac{a}{V \cos \alpha} = \frac{4a}{V \cos \alpha}$

(5)

(e)

$$\text{Weight of helicopter, } W = 9800 \text{ N}$$

✓

Required for the marks either Force (lift) = rate of change of momentum. ✓
 a statement or a recognisably formula version.

$$\frac{\Delta p}{\Delta t} = \frac{\Delta (mV)}{\Delta t} = V \frac{\Delta m}{\Delta t}$$

$$m = \rho V$$

$$\therefore \frac{\Delta p}{\Delta t} = V \rho \frac{\Delta V}{\Delta t} \\ = V^2 \rho A$$

$$\therefore W = V^2 \rho A$$

✓

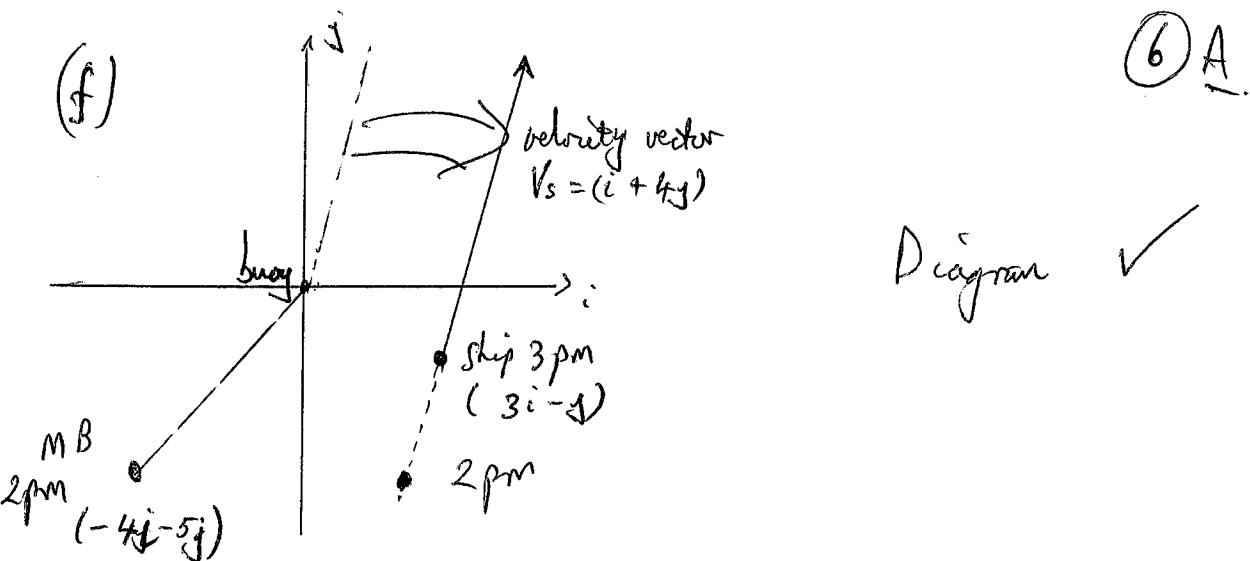
✓

$$\therefore V^2 = \frac{W}{\rho A} = \frac{9800}{1.2 \times 10^3 \pi \times 3^2} \\ = 288$$

$$\underline{V = 17 \text{ m s}^{-1}}$$

✓

(5)

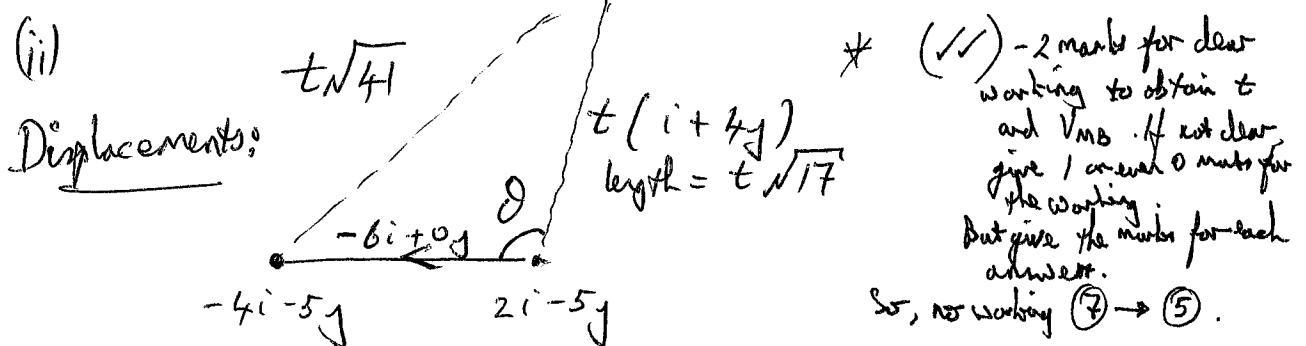


(i) Position of ship at 2 pm is vector position at 3 pm - 1 hour $\times V_s$ ✓

$$= 3i - j - 1(i + 4j)$$

$$= \underline{2i - 5j}$$

✓



Using the sine rule, $t^2 41 = 36 + t^2 17 - 2t\sqrt{17} \cdot \sqrt{36} \cdot \cos \theta$

and $\cos \theta = \frac{\underline{a} \cdot \underline{b}}{|a||b|} = \frac{(8i + 0j) \cdot t(i + 4j)}{\sqrt{36} \cdot t\sqrt{17}}$

$$= \frac{-6t}{\sqrt{36} \cdot t\sqrt{17}}$$

$$= -\frac{1}{\sqrt{17}}$$

$\therefore 41t^2 = 36 + 17t^2 + 2t\sqrt{17} \cdot \sqrt{36} \cdot \frac{1}{\sqrt{17}}$

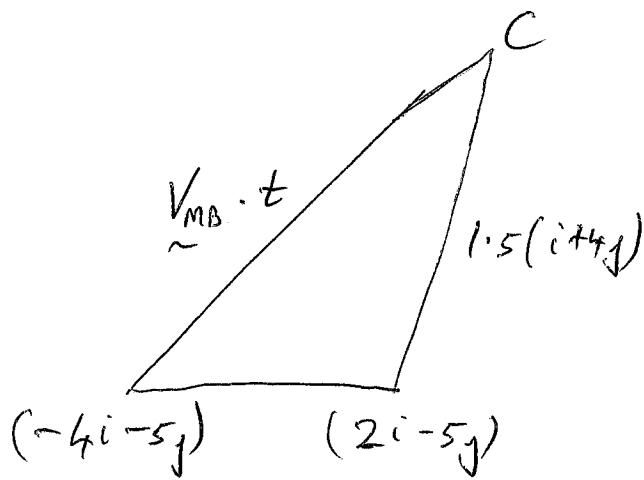
$$24t^2 = 36 + 2 \cdot 6t$$

$$2t^2 - t - 3 = 0$$

$$t = \frac{1 \pm \sqrt{1+24}}{4} = \frac{1}{4} \pm \frac{5}{4} \Rightarrow t = \frac{1.5}{1} \text{ hr}$$

i.e. interception at 3:30 pm ✓

⑥ B



point C is at: $2i - 5j + 1.5(i + 4j)$
i.e., $(3.5i + j)$

so that $V_{MB} \times 1.5 = (3.5i + j) - (-4i - 5j)$

$$V_{MB} \times 1.5 = 7.5i + 6j$$

$$V_{MB} = 5i + 4j \quad \checkmark$$

check: $|V_{MB}| = \sqrt{5^2 + 4^2}$ (7)

$$= \sqrt{41}.$$
 as given in question.

or $V_{MB} = a i + b j.$

Ship and boat end up at the same point after time t.
 \therefore Add the respective velocities to the 2pm start points.

Hence $-4i - 5j + t(ai + bj) = 2i - 5j + t(i + 4j)$

Given $t(a-1)i + t(b-4)j = 6i + 0j$ ship

equating for i: $t(a-1) = 6$

... " j: $t(b-4) = 0 \Rightarrow b = 4$

but we know (given) $|V_{MB}| = \sqrt{41}$

So $a^2 + b^2 = 41$ with $b = 4$.

$a = \pm 5$. But t is positive so $a = +5$

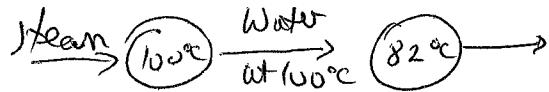
$V_{MB} = 5i + 4j$, with $\frac{t = 1.5}{(+2pm)}$

(7)



For water : $\Delta Q_w = mc\Delta T$

$$\begin{aligned}\Delta Q_w &= 1 \times 4200 \times (60 - 38) \\ &= 92400 \text{ J}\end{aligned}$$



For condensing steam,

$$\begin{aligned}\Delta Q &= mL + mc\Delta T \\ &= m(L + c\Delta T)\end{aligned}$$

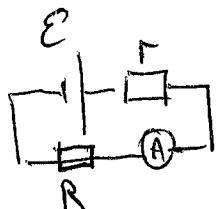
Require, $92400 = m(2.26 \times 10^6 + 4200(100 - 82))$ ✓

* If $mc\Delta T$ term left out
to give 40.9 g then loss
1 mark.

$$m = \frac{92400}{(2.26 \times 10^6 + 4200 \times 18)} = \frac{92400}{2.26 \times 10^6 + 75600}$$

$$m = 39.6 \text{ g} = 40 \text{ g} = 0.040 \text{ kg}$$

(h)



$$E = Ir + IR$$

(4)

✓ equation in symbols
or values.

$$\begin{aligned}\text{For } R = 2.0 \Omega, E &= 0.8r + 0.8 \times 2 \\ &= 0.8r + 1.6\end{aligned}$$

$$\text{For } R = \frac{10}{7} \Omega, E = 1.0r + \frac{10}{7}$$

✓ simultaneous
equations.

$$R_{II} : \frac{1}{R_{II}} = \frac{1}{5} + \frac{1}{2}$$

$$R_{II} = \frac{10}{7} \Omega$$

$$= 1.4(3) \Omega$$

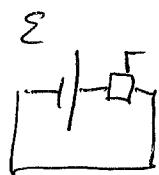
$$\text{Subtracting, } 0 = -0.2r + 1.6 - 1.0$$

$$r = \frac{6}{7} \Omega = 0.86 \Omega$$

$$E = \frac{16}{7} V = 2.3 V$$

(5)

(i)



shorted.

(8)

$$I = \frac{E}{R} \Rightarrow I = \frac{6}{R}$$

$$\text{or } R = 2 \Omega$$

$$\frac{dP_R}{dR} = \frac{d}{dR} \frac{E^2 R}{(R+R)^2} = 0 \\ \Rightarrow R = r$$

Then $I = \frac{E}{R+r} = \frac{6}{4} = 1.5 A$

$$\begin{aligned} \text{Power} &= I^2 R \\ &= 1.5^2 \times 2 \\ &= 4.5 W \end{aligned}$$

Energy dissipated externally in 1 minute is 60×4.5

$$= \underline{\underline{270}} \text{ J}$$

(4)

(j)

$$f = \frac{c}{\lambda} = \frac{3 \times 10^8}{639 \times 10^{-9}} = 4.69 \times 10^{12} \text{ Hz.}$$

$$E_{\text{photon}} = hf = 6.63 \times 10^{-34} \times 4.69 \times 10^{12} \\ = 3.11 \times 10^{-19} \text{ J}$$

$$N_{\text{photon per nanowatt}} = \frac{\text{power} \times \text{time}}{E_{\text{photon}}} \quad \checkmark$$

$$= \frac{0.5 \times 10^{-3} \times 10^{-9}}{3.11 \times 10^{-19}}$$

$$= \underline{\underline{1.6 \times 10^6}}$$

(3)

(9)

(k)



NII.

$$T_{top} + mg = \frac{mV_{top}^2}{r} \text{ (inwards)} \quad \checkmark$$

$$T_{top} = 0 \Rightarrow mg = \frac{mV_{top}^2}{r}$$

$$V_{top} = \sqrt{rg}$$



$$T_{bottom} - mg = \frac{mV_{bottom}^2}{r}$$

$$\text{Energy Cons. } \frac{1}{2}mV_{top}^2 + mg\cdot 2r = \frac{1}{2}mV_{bottom}^2 \quad \checkmark$$

$$\begin{aligned} V_{bottom}^2 &= V_{top}^2 + 4gr \\ &= 5g + 4g \\ &= 5g \end{aligned}$$

$$\begin{aligned} \therefore T_{bottom} &= m \cdot \frac{5g}{r} + mg \\ &= 6mg \end{aligned}$$

*R if wrong but correctly added
give this final mark.*

(6)

(l)

$$\text{For SHM, } x = A \sin(\omega t)$$

$$V = Aw \cos(\omega t)$$

$$a = -Aw^2$$

Sand loses contact when the minimum value of the acceleration is equal to g .

$$\therefore g = Aw^2$$

$$f_{min}^2 = \frac{g}{4\pi^2 A}$$

$$f_{min}^2 = \frac{g \cdot 81}{4\pi^2 \times 2 \times 10^{-4}} \quad , \quad f_{min} = 35(2) \text{ Hz.}$$

(3)

(10)

(M)

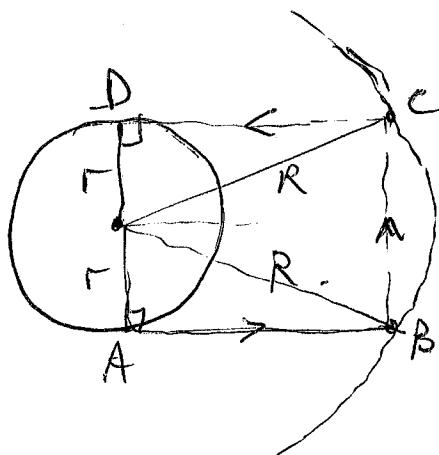


diagram ✓

tangential paths. ✓

$$R = 3.59 \times 10^4 + 6370 \text{ km} \\ = 4.227 \times 10^4 \text{ km}$$

$$A \Delta C D = l = 2 \sqrt{R^2 - r^2} + 2r \quad (AB + AC) \quad (BC) \quad \checkmark$$

$$l = 2 \sqrt{4.28^2 \times 10^8 - 6370^2} + 2 \times 6370 \text{ km}$$

If R taken as $3.59 \times 10^4 \text{ km}$
then $= 2 \times 41.8 \times 10^3 + 2 \times 6370 \text{ km}$
 $= 9.63 \times 10^7 \text{ m}$

$$l = 2 \sqrt{3.59^2 \times 10^8 - 6370^2} + 2 \times 6370 \\ = 8.34 \times 10^7 \text{ m.} \\ = \underline{8.3 \times 10^7 \text{ m.}}$$

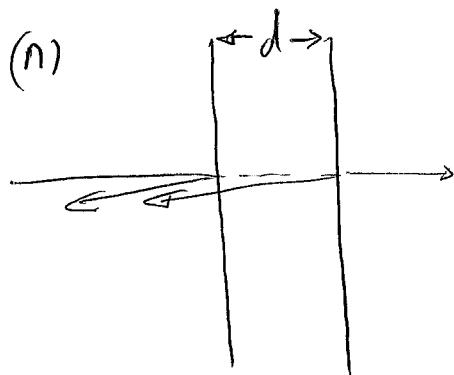
With $\Delta t = \underline{6.285}$

$$\Delta t = \frac{l}{c} = \frac{9.63 \times 10^7}{3 \times 10^8} \\ = \underline{0.321 \text{ s}}$$

Max. of 5 Marks total.

(6)

(11)



(n)

For constructive interference, path difference = $m\lambda$
 (M-integer)

There will be a phase difference of π at each reflecting surface, which means that there is no phase difference introduced overall.

$$\therefore 2d = m\lambda$$

λ is decreased in the medium by a factor $\frac{1}{n}$.

Hence $\lambda = \frac{n \lambda_0}{m}$

$$\text{For } m=1, \lambda = \frac{1.52 \times 2 \times 0.42 \times 10^{-6}}{1}$$

$$= 1.28 \times 10^{-6} \text{ m} = 1280 \text{ nm}$$

IR.

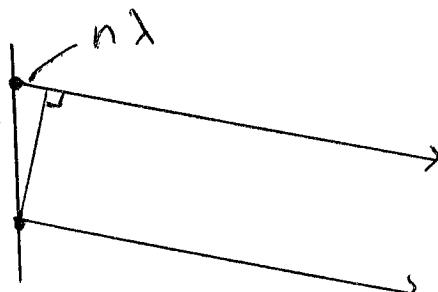
$$\text{For } m=2, \lambda = 638 \text{ nm.}$$

Visible.

(5).

(12)

(o)



Mesurment
(constructive
interference)

A path difference change of λ gives one fringe shift.

$\therefore \dots \therefore 25\lambda \therefore 25$ fringe shift ✓

In the 5 cm tube, there are $N\lambda$ length of wave. ✓

In the vacuum in the tube there are $(N-25)\lambda$ length of wave. ✓

as the wavelength is shorter in air, longer in a vacuum,
(speed of light is slightly less in air).

$$\text{Optical path} \text{ is } (N-25)\lambda_{\text{vac}} = N\lambda_{\text{air}} = N \frac{\lambda_{\text{vac}}}{n}$$

$$\therefore N-25 = \frac{N}{n}$$

$$n = \frac{N}{N-25}$$

$$\text{and } N = \frac{5 \times 10^{-2}}{600 \times 10^{-9}} \text{ m} = 8.333 \times 10^4$$

$$\text{which gives } n = 1.0003 \quad (= 1 + 3 \times 10^{-4}) \quad \checkmark$$

OR

$$25 \text{ fringes} = \frac{5 \text{ cm}}{\lambda/n} - \frac{5 \text{ cm}}{\lambda} = \cancel{5 \text{ cm}}$$

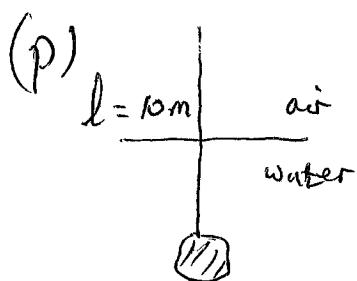
$$= \frac{5 \times 10^{-2}}{600 \times 10^{-9}} (n-1)$$

$$3000 \times 10^{-7} = n-1$$

$$\underline{n = 1.0003}$$

(5)

(13)



$$A = 5.0 \text{ cm}^2$$

$$\text{Young's Law: } F = \frac{F}{A} \cdot \frac{l}{\Delta l} \Rightarrow \Delta l = \frac{Fl}{E \cdot A}$$

In air, $\Delta l = \frac{mg \cdot l}{E \cdot A}$ ✓
Correct equation
or values (see below)

In water, upthrust is given by $\rho_w \cdot V_{\text{sub}} \cdot g$ (weight of water displaced), ✓

ρ_w = density of water

ρ_{sub} = density of submerged wreck

$$\text{Upthrust} = \rho_w \cdot \frac{M_{\text{sub}} \cdot g}{\rho_{\text{sub}}} \quad \checkmark$$

Since $\Delta l \propto$ tension,

the change in extension Δe ~~is proportional to~~ change in load

Δe i.e. the upthrust.

$$\text{so } \Delta e = \left(\frac{\rho_w}{\rho_{\text{sub}}} \cdot M_{\text{sub}} \cdot g \right) \cdot \frac{l}{E \cdot A} \quad \checkmark$$

$$= \frac{1000}{8000} \times 1 \times 10^4 \times 9.81 \times \frac{10}{5 \times 10^9 \times 5 \times 10^{-4}}$$

$$= \underline{4.9 \times 10^{-3} \text{ m}} \quad \checkmark$$

O/P load in air = $9.81 \times 10^4 \text{ N}$ ✓ (5)

$$\text{extension in air} = 39.24 \times 10^{-3} \text{ m} \quad \checkmark$$

$$\text{extension in water} = \text{extension in air} - \text{upthrust} \quad \checkmark$$

$$= 34.3 \times 10^{-3} \text{ m} \quad \checkmark$$

$$\text{difference} = \underline{4.9 \times 10^{-3} \text{ m}} \quad \checkmark$$

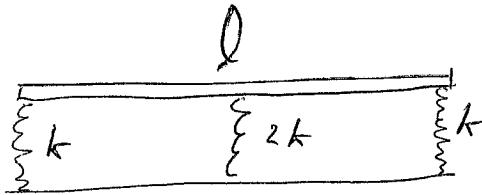
$$\text{Volume of wreck} = 1.25 \text{ m}^3$$

$$\text{Upthrust} = 12,250 \text{ N}$$

$$\text{Weight} = 98,000 \text{ N}$$

(14) A.

(q) (i)



Symmetric arrangement, so load beam ✓

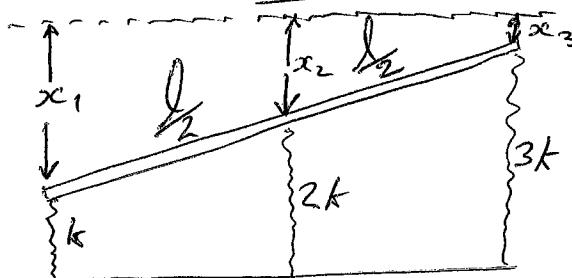
Total load, "compressive force = kx "

$$\text{so } Mg = kx + 2k \cdot x + kx \\ = 4kx$$

Thus, $x = \frac{Mg}{4k}$

$$F_{\text{left}} = F_{\text{right}} = \frac{Mg}{4} \\ F_{\text{centre}} = \frac{Mg}{2} \quad \boxed{}$$

(ii)



$$\text{Total load, } Mg = k_1 x_1 + 2k_2 x_2 + 3k_3 x_3 \quad \boxed{1} \quad \checkmark$$

Relate x_1, x_2, x_3 .

~~$$\text{Board is linear : } x_1 - x_3 = 2(x_2 - x_3)$$~~

~~$$2x_2 = x_1 + x_3 \quad \boxed{2}$$~~

~~$$\text{Take moments about centre : } \frac{Mg \cdot \frac{l}{4}}{2} - \frac{l}{2} \cdot k x_1 - \frac{Mg \cdot \frac{l}{4}}{2} + \frac{l}{2} \cdot 3k x_3 = 0$$~~

(+) ↓

~~$$\text{so, } x_1 = 3x_3 \quad \boxed{3} \quad \checkmark$$~~

~~$$\text{Eliminating } x_1 \text{ in } \boxed{2} \text{ and } \boxed{3}, \quad x_2 = 2x_3 \quad \boxed{4}$$~~

$$\text{so } Mg = k \cdot 3x_3 + 2k \cdot 2x_3 + 3k \cdot x_3$$

Here you need
values of x_1, x_2, x_3

not F_1, F_2, F_3
since $F_1 = F_2 = F_3$.

$$x_3 = \frac{Mg}{10k} \quad \boxed{5} \quad F_3 = \frac{3}{10} Mg$$

$$x_2 = \frac{2}{10} \cdot \frac{Mg}{k} \quad \boxed{6} \quad F_2 = \frac{4}{10} Mg$$

$$x_1 = \frac{3}{10} \cdot \frac{Mg}{k} \quad \boxed{7} \quad F_1 = \frac{3}{10} Mg$$

$(F_1 + F_2 + F_3 = Mg)$

(8)

(q) continued.

Equations needed are

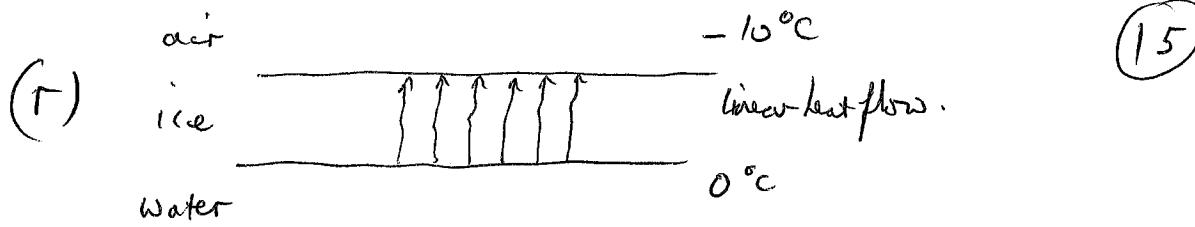
- eque. ① total load
- ② Beam is linear
- ③ moments about centre.

- or
- moments about LH end. $\frac{Mg}{2} = kx_2 + kx_1$
 - moments about RH end $\frac{Mg}{2} = 3kx_3 + kx_2$
which will give $x_1 = 3x_3$
 - and the Beam is linear ②.

- ~~or~~
- moments above one end
 - moments about centre
 - Beam is linear

- ~~or~~
- total load
 - moments about one end
 - Beam is linear

The fact that the beam is linear ② is required in all derivations.



$$P = \frac{\Delta Q}{\Delta t} + \lambda A \left(\frac{T_H - T_c}{x} \right) \quad (1)$$

Now, $P = \frac{m h}{t}$

$$= \rho A \frac{\Delta x}{\Delta t} \cdot L \quad (2)$$

Equating power flow given by (1) and (2)

$$\cancel{\rho A \frac{\Delta x}{\Delta t}} = \lambda A \cancel{\frac{(T_H - T_c)}{x}} \quad x \rightarrow \text{a finite thickness.} \quad \checkmark$$

$\lim_{\Delta x \rightarrow 0, \Delta t \rightarrow 0} \rho L x \Delta x = \lambda (T_H - T_c) \Delta t.$

$$L \rho \int_{\infty}^{x_2} x dx = \lambda (T_H - T_c) \int_{t_1}^{t_2} dt$$

$$L \rho \frac{1}{2} (x_2^2 - x_1^2) = \lambda (T_H - T_c) (t_2 - t_1) \quad \checkmark$$

$$t_2 - t_1 = \frac{L \rho}{2 \lambda} \cdot \frac{(x_2^2 - x_1^2)}{(T_H - T_c)}$$

$$= \frac{330 \times 10^3 \times 900}{2 \times 2.1} \cdot \frac{(10 \times 10^{-2})^2 - (5 \times 10^{-2})^2}{(0 - -10)} \quad \checkmark$$

$$= \frac{330 \times 10^3 \times 900}{4 \times 2 \times 10} \cdot (75 \times 10^{-4})$$

$$= 53.0 \times 10^3 \text{ s}$$

$$= 884 \text{ minutes}$$

$$= 14.7 \text{ hours.}$$

(7)

(16)

Ques 2 (a) $f = 50 \text{ Hz}$, $I_{\text{rms}} = 10^{-6} \text{ A}$, diameter = 1 mm
free electrons cm^{-3} is 9×10^{22}

$$I_{\text{max}} = n A v e \quad I_{\text{max}} = \sqrt{2} \cdot 10 \quad \checkmark$$

$$10 \sqrt{2} = 9 \times 10^{22} \times 10^{-6} \times \pi \left(\frac{1}{2}\right)^2 \times V \times 1.6 \times 10^{-19} \quad \checkmark$$

$$V = \frac{10 \sqrt{2}}{9 \times 10^{22} \pi \times 1.6 \times 10^{-19}} \quad \checkmark$$

$$V_{\text{max}} = 1.25 \times 10^{-3} \text{ m s}^{-1}$$

AC $V = V_0 \sin(\omega t)$ or $\cos(\omega t + \phi)$, etc.
 $= A \omega \sin(\omega t)$

$$V_{\text{max}} = A \omega$$

$$A = \frac{V_{\text{max}}}{2\pi f} \quad \omega = 2\pi f \quad \checkmark$$

$$= \frac{1.25 \times 10^{-3}}{2\pi \times 50}$$

$$A = \underline{3.98 \times 10^{-6} \text{ m}} \quad \checkmark$$

(6)

(b) $R = \rho \frac{l}{A}$, $R' = \rho \frac{l'}{A'}$ \checkmark

With V constant $\Rightarrow A' l' = A l$. \checkmark

$$\text{Required } \frac{R}{R} = \frac{R' - R}{R} = \left(\rho \frac{l'}{A'} - \rho \frac{l}{A} \right) / \rho \frac{l}{A} \quad \checkmark$$

$$= \frac{l'}{l} \cdot \frac{A}{A'} - 1$$

$$= \frac{l'}{l} \cdot \frac{A}{(Al)/l'} - 1 = \frac{l'^2}{l^2} - 1$$

But $l' = l + \epsilon$, so $\frac{R}{R} = \frac{(l^2 + 2\epsilon l + \epsilon^2)}{l^2} - 1$

(17)

$$\frac{\delta R}{R} = \frac{2\epsilon}{l} + \frac{\epsilon^2}{l^2} \quad \text{neglect 2nd term. in } \frac{\epsilon^2}{l^2}$$

$$\text{so } \frac{\delta R}{R} \approx \frac{2\epsilon}{l}$$

$$\text{Hence } \delta R = 2 \times 0.001 \times 100.0$$

$$= 0.2 \Omega$$

$$\text{and } R' = \underline{100.2 \Omega}$$

(6)

Or for example, $R = \frac{\rho l}{A}$

$$\delta R = \rho \frac{\delta l}{A} + \rho l \frac{\delta A}{A^2}$$

$$V = Al$$

$$\delta V = A \delta l + l \delta A$$

$$\text{so that } \delta A = - A \frac{\delta l}{l}$$

$$\text{Hence } \delta R : \rho \frac{\delta l}{A} + \rho l \cdot \left(A \frac{\delta l}{l} \right)$$

$$= \rho \frac{\delta l}{A} + \rho \frac{\delta l}{A}$$

$$= 2\rho \frac{\delta l}{A}$$

$$= 2 \cdot R \cdot \frac{\delta l}{l}$$

$$= 2 R \cdot \frac{\epsilon}{l}$$

$$= \underline{0.2 \Omega}$$

$$R' = \underline{100.2 \Omega}$$

(18)

(C)

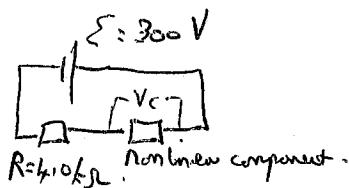


Diagram or indication
of the correct circuit used

$$E = IR + V_c$$

$$\text{and } I = AV_c + BV_c^2$$

$$E = RAV_c + RBV_c^2 + V_c$$

$$E = (RA+1)V_c + RBV_c^2$$

quadratic in V_c with other terms given

$$RBV_c^2 + (RA+1)V_c - E = 0$$

$$V_c = \frac{-(RA+1) \pm \sqrt{(RA+1)^2 + 4RB.E}}{2RB}$$

$$= \frac{-(0.28+1) \pm \sqrt{[1.28^2 + 4 \cdot 4.0005 \cdot 300]}}{2 \times 4 \times 0.005}$$

(A, B given in mA).

$$= \frac{-1.28 \pm \sqrt{1.28^2 + 24}}{0.04}$$

$$= \underline{94.6} \text{ V} \quad (\text{take + sign}).$$

$$I = AV_c + BV_c^2$$

$$= 0.070 \times 94.6 + 0.0050 \times 94.6^2$$

$$= \underline{51.4 \text{ mA}}$$

[check: $300V - 4000 \times 51.35 \times 10^{-3}V = 94.586V$].

$$E - R I = V_c$$

(6)

(19)

part(c) can also be done directly from I , although this then requires a calculation of V_c rather than obtaining an expression.

$$\text{From Kierhoff II, } V_c = 300 - 4 \times 10^3 I$$

$$\text{and with } I = A V_c + B V_c^2$$

We have,

$$I = 0.07 \times 10^{-3} (300 - 4 \times 10^3 I) + 0.005 \times 10^{-3} (300 - 4 \times 10^3 I)^2$$

$$I = 0.021 - 0.28 I + 0.005 \times 10^{-3} (300^2 + 16 \times 10^6 I^2 - 2.4 \times 10^6 I)$$

$$I = 0.021 - 0.28 I + 0.45 + 80 I^2 - 12 I$$

$$I = 0.47 - 12.28 I + 80 I^2$$

$$\text{so that } 80 I^2 - 13.28 I + 0.47 = 0$$

$$I = \frac{13.28 \pm 5.09}{160} \times 1000 \text{ mA.}$$

$$= 114.8 \text{ mA or } 51.2 \text{ mA.}$$

$$\text{Max current, } I_{\text{max}} = \frac{300 \text{ V}}{6000 \Omega} \times 1000 \text{ mA}$$

$$= 75 \text{ mA.}$$

$$\begin{aligned} \therefore I &= 51.2 \text{ mA} \\ \text{and } V_c &= 95.3 \text{ V.} \end{aligned} \quad \left. \begin{array}{l} \text{some slight} \\ \text{rounding errors evident.} \end{array} \right.$$

$$\underline{\underline{\frac{I = 51 \text{ mA}}{V_c = 95 \text{ V.}}}}$$

✓

(20)

(d)



Group of the idea by
words or diagram.

(i)

$$R = \frac{\rho l}{A}$$

$$= \frac{\rho \cdot \delta r}{2\pi r^2}$$

$$\frac{2\pi r^2}{\delta r}$$

$$\left[\text{For } \delta r \ll r, \quad R = \frac{60 \times \delta R}{2\pi (0.10)^2} \right]$$

$$R = 95 \times \delta R \text{ (r) }$$

One mark of
this approach taken.

(ii)

$$\text{In general} \quad R = \frac{\rho}{2\pi} \int_r^\infty \frac{dr}{r^2}$$

$$= \frac{\rho}{2\pi} \left[\frac{1}{r} \right]_r^\infty$$

$$= \frac{\rho}{2\pi} \left[\frac{1}{r} \right]_0^\infty$$

$$= \frac{\rho}{2\pi} \frac{1}{r}$$

$$\therefore R = \frac{60}{2\pi \cdot 0.1}$$

$$= \frac{300}{\pi} = 95.5$$

$$= \underline{\underline{95 \Omega}}$$

(7)

(21)

Qn:3.

A mark for each step, up to 9 marks. Candidates may calculate in a different order to this.

Once the tug has slowed sufficiently, its thrust of 35 kN will not allow the 50 kN break to release any more of the cable.

Neglecting any forces due to the water flowing around the tug and barge,

At moment of impact, and after, force to accelerate the

$$\text{Barge is } 50 \text{ kN}$$

$$\text{Acceleration of barge is } \frac{50 \times 10^3}{6300 \times 10^3}$$

$$a_b = \frac{1}{126} \text{ ms}^{-2}$$

$$\text{Force on the tug forwards is } (35 - 50) \times 10^3 \text{ N}$$

$$= -15 \times 10^3 \text{ N}$$

$$\text{acceleration of tug, } a_t = -\frac{15 \times 10^3}{450 \times 10^3}$$

$$= \frac{1}{30} \text{ ms}^{-2}$$

These accelerations are constant for a time t .

\therefore using "V = u + at"

$$V_{\text{barge}} = 0 + \frac{1}{126} t$$

$$\text{and } V_{\text{tug}} = 2.5 - \frac{1}{30} t$$

When $V_{\text{tug}} = V_{\text{barge}}$ then the cable is no longer slipping.

$$\therefore \frac{1}{126} t = 2.5 - \frac{1}{30} t$$

$$t = 60.6 \text{ s}$$

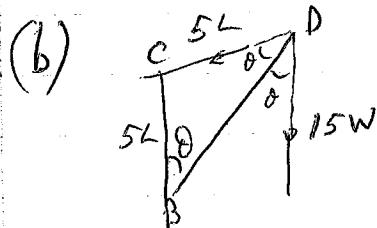
$$\text{Then } V_{\text{constant}} = \frac{60.6}{126} = \underline{\underline{0.48 \text{ ms}^{-1}}}$$

$$\text{Consequently, } S = ut + \frac{1}{2} at^2 \Rightarrow S = S_{\text{tug}} - S_{\text{barge}}$$

(22)

$$\begin{aligned}
 S &= S_{\text{tug}} - S_{\text{surge}} \\
 &= 2.5 \times 60.6 - \frac{1}{2} \cdot \frac{1}{30} (60.6)^2 - 0 - \frac{1}{2} \cdot \frac{1}{126} (60.6)^2 \\
 &= 75.7 \text{ m} \\
 &= \underline{\underline{76 \text{ m}}}
 \end{aligned}$$

(q)



Various Methods - 2 marks for method
1 mark for result

Since CB is vertical, and the cable is vertical, the angle CBD is equal to the angle between the cable and BD.

(Let $\angle CDB = \delta$) Also, $CB = CD$, so $\angle CDB = \angle CBD$
So BD bisects the angle at the top.

✓✓ Working

∴ Since BD can provide no torque,
 $15W \cos \delta = T_{CD} \cdot \cos \delta$

$$\underline{T_{CD} = 15 \text{ W}}$$

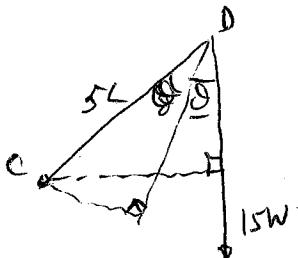
✓ result

Or using cosine rule, $(5L)^2 = (8L)^2 + (5L)^2 - 2 \cdot 5L \cdot 8L \cdot \cos \delta$
 $64 = 80 \cos \delta$

$$\cos \delta = 0.8$$

Take moments about C

$$0 = T_{BD} \cdot 5L \cdot \sin \delta - 15W \cdot 5L \sin 2\delta$$



$$\text{i.e. } T_{BD} \cdot 5L \cdot \sin \delta = 15W \cdot 5L \cdot 2 \sin \delta \cdot \cos \delta$$

$$\begin{aligned}
 T_{BD} &= 15W \cdot 2 \cdot 0.8 \\
 &= \underline{\underline{24 \text{ W}}}
 \end{aligned}$$

✓✓ Working

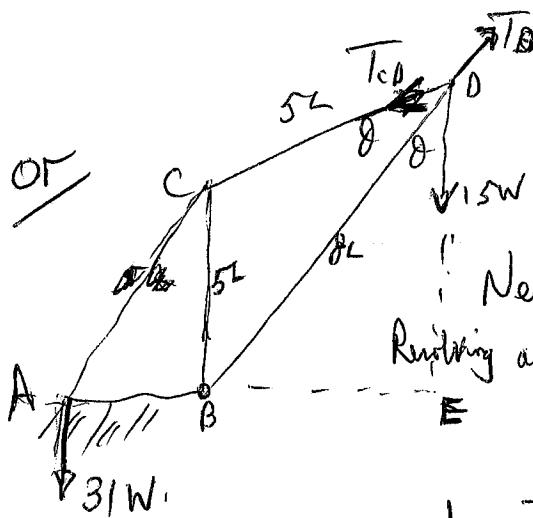
✓ result

Resolve forces on D vertically: $15W = 24W \cdot \cos \delta - T_{CD} \cdot \cos 2\delta$

$$15W = 24W \cdot 0.8 - T_{CD} \cdot 0.28$$

$$\underline{\underline{T_{CD} = 15 \text{ W}}}$$

(23)



! Newton. and if it is shown that BD bisects the angle,
Resolving along DB. $T_{CD} \sin \theta = 15 \text{ N. and}$
 $\underline{T_{CD} = 15 \text{ N.}}$

$$\text{and } T_{BD} = T_{CD} \cos \theta + 15 \text{ N. and} \\ = 2 \times 15 \text{ N.} \times 0.8 \\ = \underline{24 \text{ N.}}$$

(iii) Distance AB.

Take moments about B.

$$\omega \theta = 0.8$$

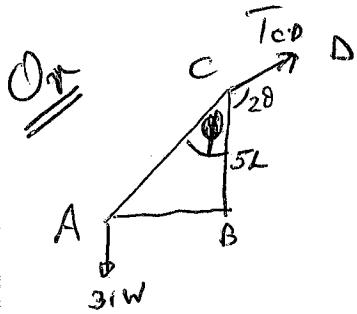
$$31W \times AB = 15W \times BE$$

$$\omega \theta = 0.6.$$

$$31W \times AB = 15W \times 8L \sin \theta$$

$$AB = \frac{15}{31} \times 8L \times 0.6 = 2.32L$$

working + result.
 ✓ ✓ (8)



Resolving horizontal forces on C.

$$T_{CD} \cos(90 - 2\theta) = T_{CA} \sin \theta$$

Resolving vertically at A.

$$31W = T_{CA} \cos \theta$$

Eliminating T_{CA} :

$$31W \cdot \sin \theta = 15W \cos(90 - 2\theta)$$

$$\text{i.e. } \tan \theta = \frac{15}{31} \cdot \sin 2\theta \quad \cdot \omega(90 - 2\theta) = \sin 2\theta$$

$$\text{So, } \tan \theta = \frac{15}{31} \cdot 2 \sin \theta \cdot \cos \theta = \frac{15}{31} \cdot 2 \cdot 0.6 \times 0.8 = 0.4645$$

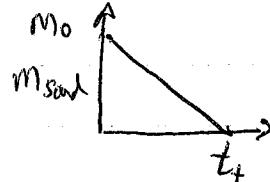
$$\text{and } \tan \theta = \frac{AB}{5L} \Rightarrow AB = 5L \tan \theta = \underline{2.32L}$$

(24)

(c)



$$\left[\begin{array}{l} M = \text{Mass of bucket} \\ M_0 = \text{initial mass of sand} \end{array} \right]$$



$$\begin{aligned} m_s &= M_0 - kt \\ &= M_0 - \frac{M_0}{t_s} \cdot t \\ &= M_0 \left(1 - \frac{t}{t_f}\right) \end{aligned}$$

$$\text{total mass lifted is, } M = M + M_0 \left(1 - \frac{t}{t_f}\right)$$

Newton II $M a = F - Mg$

(upward)

$$a = \frac{F}{M} - g$$

$$\int_0^t a dt = \int_0^V dV = V$$

$$V = \int_0^{t_f} \left(\frac{F}{M + M_0 \left(1 - \frac{t}{t_f}\right)} - g \right) dt$$

$$V = \int_0^{t_f} \frac{F}{\left(M + M_0 - \frac{M_0 \cdot t}{t_f}\right)} - \int_0^{t_f} g dt$$

$$\checkmark = - \frac{t_f}{M_0} F \left[\ln \left(M + M_0 - \frac{M_0 \cdot t_f}{t_f} \right) - \ln (M + M_0) \right] - g t_f$$

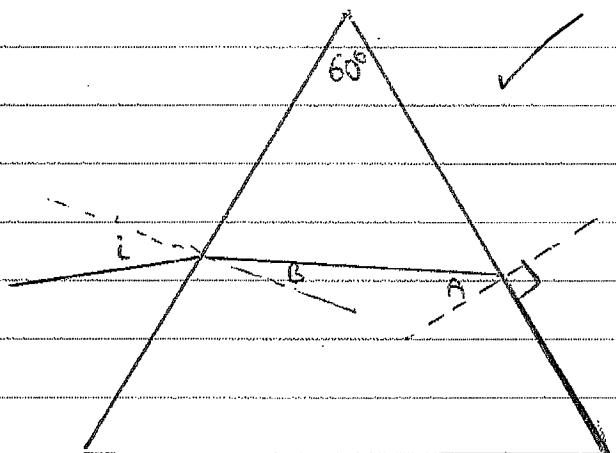
$$\checkmark = - \frac{t_f}{M_0} \cdot F \ln \left(\frac{M}{M + M_0} \right) - g t_f$$

$$\checkmark = \frac{t_f}{M_0} \cdot F \cdot \ln \left(1 + \frac{M_0}{M} \right) - g t_f$$

(d).

25

Q4. a)



$$\sin A = \frac{1}{1.5}$$

$$A = 41.81^\circ$$

$$A + B = 60^\circ \rightarrow B = 18.19^\circ$$

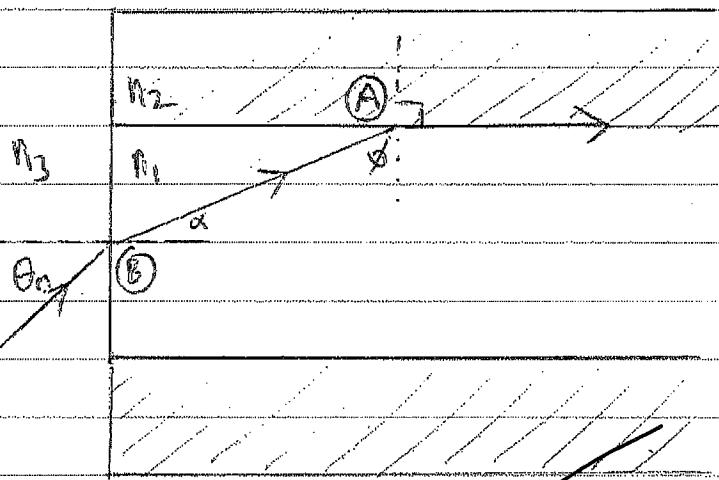
$$\frac{\sin i}{\sin 18.19^\circ} = 1.5$$

$$i = 27.92^\circ$$

(Greatest) angle, $i = 28^\circ$

(5)

b)



Suitable angles marked
on a diagram ✓

$$\text{At } A: n_1 \sin \phi = n_2 \sin 90^\circ \rightarrow \sin \phi = \frac{n_2}{n_1} \rightarrow \phi = \sin^{-1} \left(\frac{n_2}{n_1} \right)$$

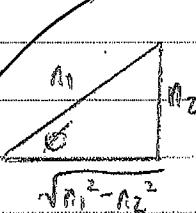
$$\alpha = 90 - \phi = 90 - \sin^{-1} \left(\frac{n_2}{n_1} \right)$$

$$\begin{aligned} n_3 \sin \theta_m &= n_1 \sin \alpha = n_1 \sin \left(90 - \sin^{-1} \left(\frac{n_2}{n_1} \right) \right) \\ &= n_1 \cos \left(\sin^{-1} \left(\frac{n_2}{n_1} \right) \right) \end{aligned}$$

$$= n_1 \cdot \sqrt{n_1^2 - n_2^2}$$

$$= \sqrt{n_1^2 - n_2^2}$$

$$\sin \theta_m = \sqrt{n_1^2 - n_2^2}$$

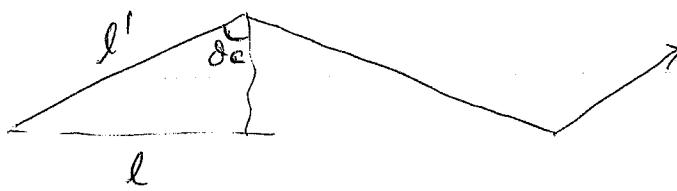


$$\left[\theta_m = \sin^{-1} \left(\frac{\sqrt{n_1^2 - n_2^2}}{n_3} \right) \right]$$

$$\text{or } \sin \theta_m = \frac{n_1}{n_3} \sqrt{1 - \frac{n_2^2}{n_1^2}}$$

(4)

(ii)



$$t_l = \frac{n_1 l}{c} = 4.953 \times 10^{-4} \text{ s}$$

$$t'_l = \frac{n_1 l}{c \sin \theta_c} = 5.053 \times 10^{-4} \text{ s.}$$

$$\sin \theta_c = 0.9802$$

$$\begin{aligned} \Delta t &= 0.100 \times 10^{-4} \text{ s} \\ &= 1.00 \times 10^{-5} \text{ s} \\ &= \underline{10 \mu\text{s}} \end{aligned}$$

(iii)

$$f_{\text{mean}} = \frac{1}{\Delta t} = \underline{99.9 \text{ kHz.}}$$

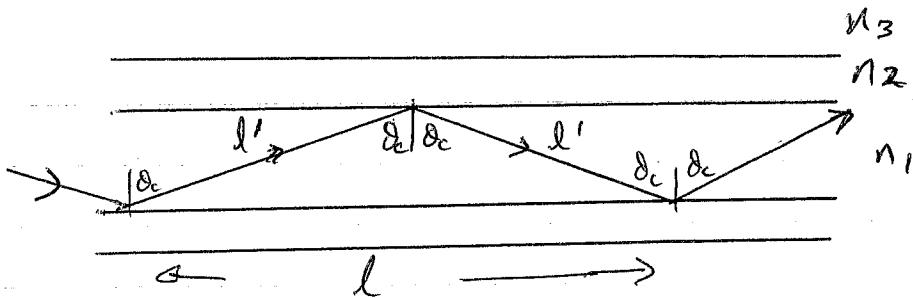
so that pulses are not overlapping.

4

parts (ii) (ii') and (iv) can be done in any order. Some will find that doing the calculation in (ii) first helps them with the algebra required in part (iv).

(27)

(iv)



In the limit of $\theta \rightarrow \theta_c$, the angle of incidence in the fibre $\rightarrow \theta_c$

2 Marks
for the
idea of
the
two
paths.

Light travelling along the core travels a distance l in time $t_{min} = \frac{n_1 l}{c}$ ✓

... $\therefore l'$ travels distance l' in $t_{max} = \frac{n_1 l}{c \sin \theta_c}$ ✓

$$\text{Since } l' = \frac{l}{\sin \theta_c}$$

$$\text{and } n_1 \sin \theta_c = n_2$$

$$\text{So } l' = \frac{l n_1}{n_2}$$

$$\text{and } t_{max} = \frac{n_1^2}{n_2} \frac{l}{c}$$

$$\text{So } \Delta t = \frac{n_1 l}{c} \left(\frac{n_1}{n_2} - 1 \right)$$

$$= \underline{\frac{l}{c'} \frac{\Delta n}{n_2}}$$

✓

(3x)

Total. (12) $\rightarrow [4+4+4]$

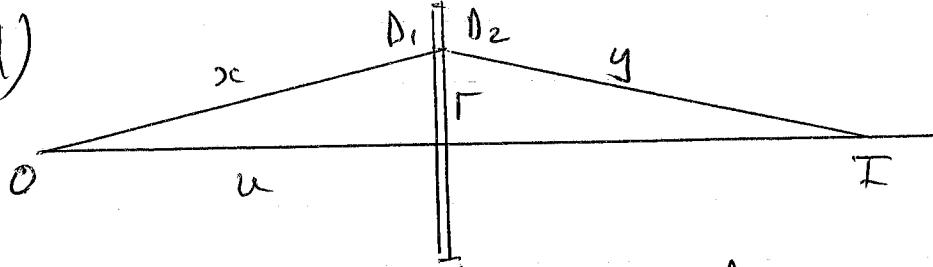
$$(c) \text{ for } \frac{1}{f} + \frac{1}{u} = \frac{1}{v}$$

$\lim_{u \rightarrow \infty}$ is $v = f$

for the object distance $\rightarrow \infty$, rays of light travelling "parallel" to the axis (2)

and so f is the distance/point from the lens at which rays from a distant object will cross / focus (on the principal axis).

(d)



We need to compare the time along the axis path OI and the path OD_1, D_1D_2, D_2I .

$$\text{Time from } O \text{ to } I \text{ along the axis, } t_1 = \frac{u}{c} + \frac{d_{A_0}}{c} + \frac{v}{c}$$

$$\text{Time along } OD_1, D_1D_2, D_2I \text{ is } t_2 = \frac{x}{c} + \frac{d_{A_0}(1-kr^2)}{c} + \frac{y}{c}$$

$$\begin{aligned} \text{Now } x^2 &= r^2 + u^2 \\ &= u^2 \left(1 + \frac{r^2}{u^2}\right) \end{aligned}$$

$$x \approx u \left(1 + \frac{1}{2} \frac{r^2}{u^2}\right)$$

$$\text{Similarly } y \approx \frac{v}{c} \left(1 + \frac{1}{2} \frac{r^2}{v^2}\right)$$

$$\text{Hence } t_2 = \frac{u}{c} \left(1 + \frac{1}{2} \frac{r^2}{u^2}\right) + \frac{d_{A_0}}{c} (1 - kr^2) + \frac{v}{c} \left(1 + \frac{1}{2} \frac{r^2}{v^2}\right)$$

$$\text{For } t_1 = t_2$$

$$\cancel{\frac{u}{c}} + \cancel{\frac{d_{A_0}}{c}} + \cancel{\frac{v}{c}} = \cancel{\frac{u}{c}} + \frac{1}{2} \frac{r^2}{u^2} + \cancel{\frac{d_{A_0}}{c}} - \cancel{\frac{d_{A_0}kr^2}{c}} + \cancel{\frac{v}{c}} + \frac{1}{2} \frac{r^2}{v^2}$$

(29)

which gives $0 = \frac{1}{2c} \frac{U^2}{u} - d n_0 k r^2 + \frac{1}{2c} \frac{r^2}{v}$

$$2 d n_0 k = \frac{1}{u} + \frac{1}{v}$$

with $2 d n_0 k$ constant

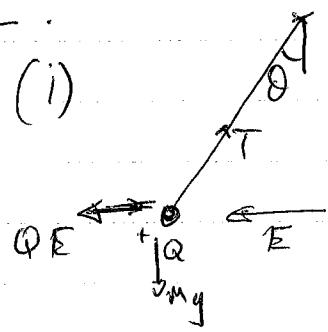
and $f = \underline{\frac{1}{2 d n_0 k}}$.

✓
(6)

(30)

Ques 5

(a) (i)

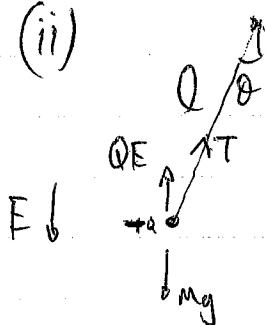


$$\text{Resolve forces: } \begin{aligned} \downarrow & \rightarrow mg - TE \cos \theta = 0 \\ & \leftarrow QE - TE \sin \theta = 0 \end{aligned}$$

$$\frac{QE}{mg} = \tan \theta$$

✓
✓

(ii)



Not in equilibrium.

Resolve \perp to string:

$$\rightarrow -QE \sin(-\theta) + mg \sin(\theta) = ma$$

and $a = l \ddot{\theta}$

$$QE \sin \theta - mg \sin \theta = ml \ddot{\theta}$$

for small θ , $\sin \theta \approx \theta$ (equivalent)

Hence ~~$(QE - mg) \theta = ml \ddot{\theta}$~~

or $-(mg - QE) \theta = ml \ddot{\theta}$

SHM.

$$\omega^2 = \frac{(mg - QE)}{ml}$$

and $T = 2\pi \sqrt{\frac{ml}{(mg - QE)}}$

✓

(iii)

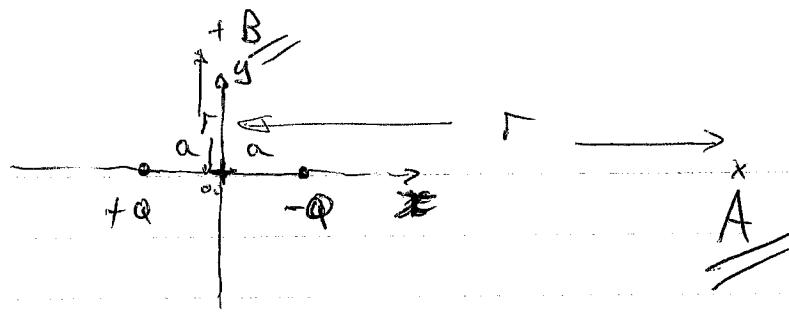
Oscillations will occur when $QE < mg$

(field is downwards, charge is negative
so electric force is upwards)

✓
(6)

(31)

(b)



(i) for point A:

$$V_A = \frac{1}{4\pi\epsilon_0} \cdot Q \left\{ \frac{1}{r+a} - \frac{1}{r-a} \right\}$$

$$= \frac{1}{4\pi\epsilon_0} \cdot \frac{Q}{r} \left\{ \frac{1}{1+\frac{a}{r}} - \frac{1}{1-\frac{a}{r}} \right\}$$

$$\approx \frac{1}{4\pi\epsilon_0} \cdot \frac{Q}{r} \left(1 - \frac{a}{r} - \left(1 + \frac{a}{r} \right) \right)$$

$$= -\frac{1}{4\pi\epsilon_0} \cdot \frac{2Qa}{r^2}$$

If the charges are $+Q \rightarrow -Q$, then

$$V \approx +\frac{1}{4\pi\epsilon_0} \cdot \frac{2Qa}{r^2}$$

(Either way is O.K.)

~~or~~ The binomial approximation may not be used;

then $V_A = \frac{1}{4\pi\epsilon_0} \cdot Q \left\{ \frac{(r-a) - (r+a)}{(r+a)(r-a)} \right\}$

$$= \frac{1}{4\pi\epsilon_0} \cdot \frac{Q}{r^2-a^2} \cdot \frac{2a}{r^2-a^2}$$

$$= \frac{1}{4\pi\epsilon_0} \cdot \frac{Q}{r^2} \cdot \frac{2a}{r^2-a^2} \quad \text{to first order in } \frac{a}{r}$$

N.B. Solution may have $k = \frac{1}{4\pi\epsilon_0}$. This is O.K.

(32)

$$\text{For } A, \quad E = \frac{1}{4\pi\epsilon_0} Q \left\{ \frac{1}{(r+a)^2} - \frac{1}{(r-a)^2} \right\}$$

$$= \frac{1}{4\pi\epsilon_0} \frac{Q}{r^2} \left[\frac{1}{(1+\frac{a}{r})^2} - \frac{1}{(1-\frac{a}{r})^2} \right]$$

$$= \frac{1}{4\pi\epsilon_0} \frac{Q}{r^2} \left\{ 1 - \frac{2a}{r} - \left(1 + \frac{2a}{r} \right)^2 \right\}$$

$$= (-) \frac{1}{4\pi\epsilon_0} Q \cdot \frac{4a}{r^3}$$

\nearrow only magnitude required, so ignore any sign.
(It does not matter if it is included)

~~$E = \frac{1}{4\pi\epsilon_0} Q \left\{ \frac{(r-a)^2 - (r+a)^2}{(r+a)^2(r-a)^2} \right\}$~~

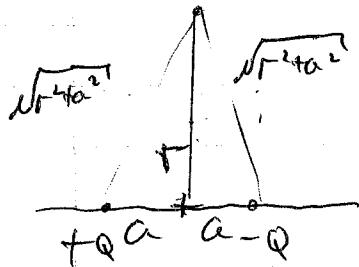
$$= \frac{1}{4\pi\epsilon_0} Q \left\{ \frac{r^2 + a^2 - 2ra - (r^2 + a^2 + 2ra)}{(r^2 - a^2)^2} \right\}$$

$$= \frac{1}{4\pi\epsilon_0} Q (-) \frac{4ra}{r^4 (1 - \frac{a^2}{r^2})^2}$$

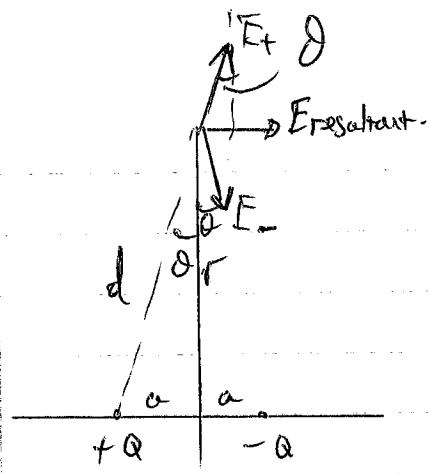
$$\approx \cancel{\frac{1}{4\pi\epsilon_0} Q \frac{4a}{r^3}} \quad \text{to first order in } \frac{a}{r}.$$

For B

$$V = \frac{1}{4\pi\epsilon_0} \cdot Q \left\{ \frac{1}{\sqrt{r+a^2}} - \frac{1}{\sqrt{r+a^2}} \right\} = 0$$



(33)



Component of E perpendicular to the line joining the charges cancel.

Resultant is parallel to the line joining the charges from to ✓

$$E_{\text{res}} = \frac{1}{4\pi\epsilon_0} \cdot \frac{Q}{d^2} \sin\theta + \frac{1}{4\pi\epsilon_0} \cdot \frac{Q}{d^2} \sin\theta$$

$$= \frac{2Q}{4\pi\epsilon_0} \cdot \frac{1}{(a^2+r^2)} \cdot \frac{a}{\sqrt{a^2+r^2}}$$

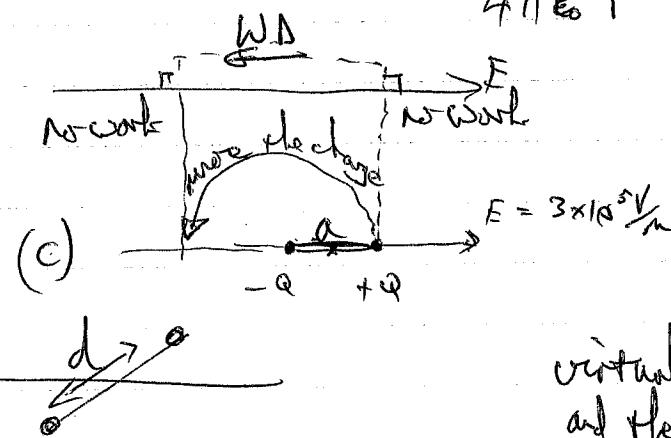
$$= \frac{2Qa}{4\pi\epsilon_0} \cdot \frac{1}{(a^2+r^2)^{\frac{3}{2}}}$$

$$= \frac{2Qa}{4\pi\epsilon_0 r^3} \left(1 + \frac{a^2}{r^2}\right)^{\frac{3}{2}}$$

$$\approx \frac{2Qa}{4\pi\epsilon_0 r^3} \left(1 - \frac{3}{2} \frac{a^2}{r^2}\right).$$

$$= \frac{2Qa}{4\pi\epsilon_0 r^3} \quad \text{to lowest order.} \quad \checkmark$$

(10)



Keep one charge fixed and move the other charge (+) against the field. Can move on a virtual path \perp to E , antiparallel to E by $2d$, and then \perp to E .

$WD = \text{force} \times \text{displacement along the field}$

$$= QE \times 2d$$

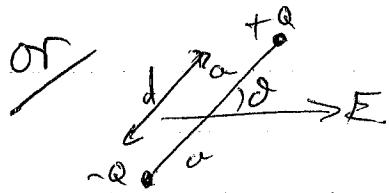
$$= \frac{2QdE}{\text{if work done by the field a sign appears.}} \quad (\text{ignore any sign})$$

Method ✓

Answer ✓ $W = 1.9(2) \times 10^{-24} \text{ J}$

(2)

(34)



$$\text{torque on dipole} = -Q E \frac{d}{2} \sin \theta - Q E \frac{d}{2} \sin \theta \\ = -Q E d \sin \theta$$

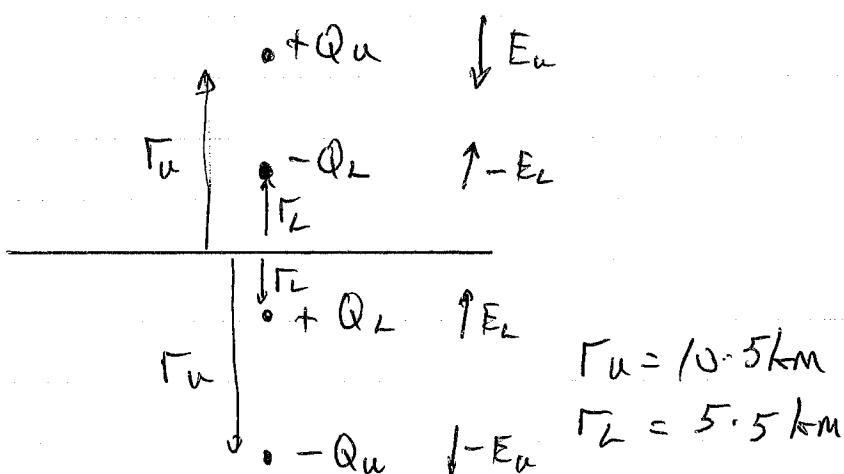
Work done on the dipole is $Q E d \sin \theta d\theta$ to rotate it through $d\theta$

$$\therefore WD = \int_0^{\pi} Q E d \sin \theta d\theta \\ = Q E d \left[-\cos \theta \right]_0^{\pi} \\ = -Q E d (-1 - 1) \\ = \underline{2 Q E d}$$

$$\therefore W = 1.92 \times 10^{-24} \text{ J}$$

(d) upper cylinder. $Q_u = n \cdot \pi r^2 h$.
 $= 0.21 \times 10^{-9} \times \pi \times 5000^2 \times 3000$
 $\underline{= 49.5 \text{ C.}}$

lower cylinder $Q_L = (20.18 \times 10^{-9}) \pi \times 3000^2 \times 7000$
 $\underline{= 99.0 \text{ C}}$



(35)

$$\text{Field at the surface, } E_s = \frac{1}{4\pi\epsilon_0} \left[+\frac{Q_u}{r_u^2} - \frac{Q_L}{r_L^2} - \frac{Q_L}{r_L^2} + \frac{Q_u}{r_u^2} \right].$$

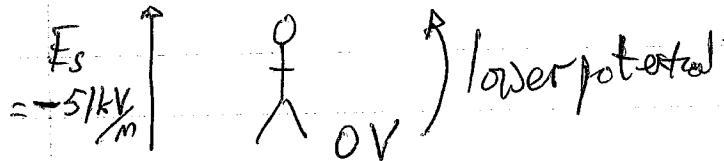
Sign: ↓ down is positive field

$$E_s = \frac{1}{4\pi\epsilon_0} \left(2 \frac{Q_u}{r_u^2} - 2 \frac{Q_L}{r_L^2} \right)$$

$$E_s = 9 \times 10^9 \times 2 \left(\frac{49.5}{10500^2} - \frac{99.0}{5500^2} \right)$$

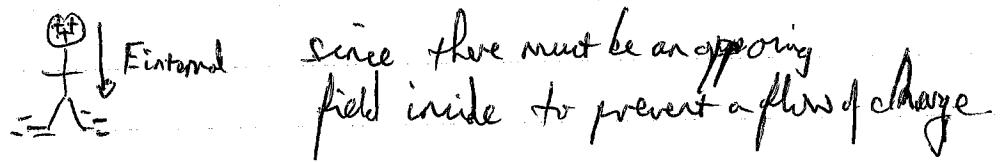
$$E_s = (-) 50.8 \text{ kV m}^{-1}$$

$$-102 \text{ kV.}$$



The potential at the head is -102 kV.

As the person is a conductor, it may be illustrated



So answer may be given as head is more positive than the feet.

(7)

Question 6

(a) If source stationary, $f \Delta t$ waves emitted in Δt .

Boat receiver $f \Delta t$ waves + $\frac{u \Delta t}{\lambda}$ waves due to its movement.

$$\therefore f' \Delta t = f \Delta t + \frac{u \Delta t}{\lambda}$$

$$\text{with } f \cdot \lambda = c$$

$$f' = f + \frac{u}{c/f}$$

$$f' = f \left(1 + \frac{u}{c}\right) = f \left(\frac{u+c}{c}\right). \quad (\text{No mark for the answer}).$$

or relative velocity between the waves and the boat moving towards
then is $u+c$

$$\text{so } f' = \frac{(u+c)}{\lambda}$$

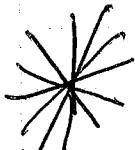
$$f \cdot \lambda = c$$

$$= \left(\frac{u+c}{c}\right) f$$

or time taken for boat to travel from crest to crest,

$$\Delta t = \frac{\text{distance}}{\text{relative speed}} = \frac{\lambda}{u+c} = \frac{c}{f(u+c)}$$

$$\therefore f = f \left(\frac{u+c}{c}\right)$$



Any method will do, but it must be clear to the marker.

A set of mixed up symbols and the given answer
will NOT do.

(4)

(37)

(b) (i) $s \rightarrow v_s$ In time Δt , $f \cdot \Delta t$ waves emitted by source.These fit in a length $(c - u) \cdot \Delta t$

$$\lambda = \frac{(c - u) \Delta t}{f \Delta t}$$

$$= \frac{c - u}{f}$$

But this shorter λ is detected by the observer as a higher frequency

$$\frac{c}{f'} = \frac{(c - u)}{f}$$

for $f' = f \frac{c}{(c - u)}$

Show that must be a derivation. No marks for the answer itself, as it is given in the question.

(ii) Source moves away $v_s \rightarrow -v_s$.
 $v_s = \frac{c}{2}$

$$f' = \frac{f}{1 + \frac{1}{2}}$$

$$f' = \frac{2}{3}f$$

$$\therefore \Delta f = \frac{2}{3}f - f$$

$$= -\frac{1}{3}f$$

Value and lower frequency
or the sign.

(ii). oppose: $f' \approx f(1 + \frac{v_s}{c})$

$$\therefore f' - f = f \frac{v_s}{c}$$

$$\frac{\Delta f}{f} \approx \frac{v_s}{c}$$

(6)

(38)

$$\text{or } f'(1 - \frac{v_s}{c}) = f$$

$$f' - f' \frac{v_s}{c} = f$$

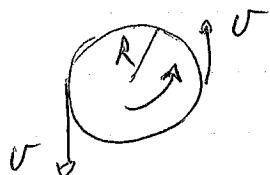
$$f' - f = f' \frac{v_s}{c}$$

$$f' - f = f \left(\frac{v_s}{c} \right) \frac{1}{1 - \frac{v_s}{c}}$$

$$\frac{\Delta f}{f} \approx f \frac{v_s}{c}$$

$$\frac{\Delta f}{f} \approx \frac{v_s}{c}$$

(c)(i)



$$v = \frac{2\pi R}{T}$$

for $v \ll c$ speed of light

*stated
opposite*

✓

✓

$$\frac{\Delta f}{f} \approx \frac{v}{c}$$

$$\Delta f = \frac{2\pi R}{T} \frac{f}{c}$$

(ii)

$$\frac{\Delta f}{f} = \frac{2\pi}{T} \cdot \frac{R}{c}$$

$$M = \frac{4}{3}\pi R^3$$

$$P = 6.99 \times 10^6 \text{ m.}$$

✓

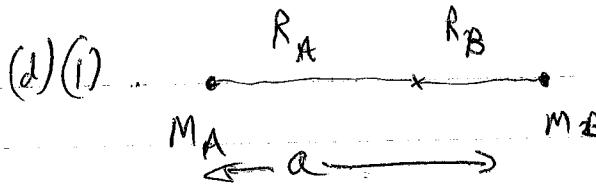
✓

$$\frac{\Delta f}{f} = 6.99 \times 10^{-6}$$

✓

(5)

(39)



The two stars have the same angular velocity, ω .
Centrifugal force about C of M is provided by gravity.

$$\therefore M_A R_A \omega^2 = G \frac{M_A M_B}{a^2}$$

$$\text{and } M_B R_B \omega^2 = G \frac{M_A M_B}{a^2}$$

$$\therefore R_A \omega^2 = G \frac{M_B}{a^2}$$

$$\text{and } R_B \omega^2 = G \frac{M_A}{a^2}$$

$$\text{Adding } \omega^2 (R_A + R_B) = G \frac{(M_A + M_B)}{a^2} \quad \checkmark$$

$$\omega^2 a = G \frac{M}{a^2}$$

$$\frac{4\pi^2}{T^2} = G \frac{M}{a^3}$$

$$\text{or } T^2 = \frac{4\pi^2 \cdot a^3}{G M} \quad \overrightarrow{\text{Do not allow straight}}$$

$\frac{m v^2}{R} = \alpha \frac{m M}{R^2}$ here
 use Kepler III for a central
 orbit (3)

(ii) $M = \frac{4\pi^2}{G T^2} a^3$

$$= \frac{4\pi^2}{6.67 \times 10^{-11}} \cdot \frac{(19.8 \times 1.5 \times 10^{11})^3}{(50.1 \times 365 \times 24 \times 3600)^2}$$

$$= 6.21 \times 10^{30} \text{ kg}$$

✓

(1)

(40)

(iii) Centrifugal force due to gravity.

$$\frac{M_A V_A^2}{R_A} = \frac{G M_A M_B}{a^2}$$

Since $V_A = \frac{2\pi R_A}{T}$

then $\frac{V_A \cdot 2\pi R_A}{T} = \frac{GM_B}{a^2}$

so $\underline{V_A = \frac{GM_B \cdot T}{2\pi a^2}}$

(2)

(iv) $\frac{\Delta t}{f} = \frac{V_A}{c} = \frac{GM_B \cdot T}{2\pi a^2 c}$

so $M_B = \frac{2\pi a^2 c \cdot \Delta t}{f G T}$

$M_B = 5.65 \times 10^{30} \text{ kg}$

✓

Total mass found from $T^2 = \frac{4\pi^2}{GM} \cdot a^3$ in part (ii)

to give $M_A = 6.2 \times 10^{30} - 5.65 \times 10^{30}$

$M_A = 5.6 \times 10^{29} \text{ kg}$

(3)

(v) No external torque, or in the zero-momentum frame, etc.

$$M_A R_A = M_B R_B$$

$$\therefore \frac{R_A}{R_B} = \frac{M_B}{M_A}$$

$$= 10 \cdot (1)$$

✓ (1)

10